

# Performance analysis of coated plutonia particle fuel compact for radioisotope heater units

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Received 6 October 2000; received in revised form 8 December 2000; accepted 24 January 2001

## Abstract

Coated plutonia particle fuel has been proposed recently for use in radioisotope power systems and radioisotope heater units for a variety of space missions requiring power levels from milliwatts to tens or even hundreds of watts. The  $^{238}\text{PuO}_2$  fuel kernels are coated with a strong layer of ZrC designed to fully retain the helium gas generated by the radioactive decay of  $^{238}\text{Pu}$ . A recent investigation has concluded that helium retention in large-grain ( $\geq 200\ \mu\text{m}$ ) granular and polycrystalline fuel kernels is possible even at high-temperatures ( $> 1700\ \text{K}$ ). Results of performance analysis showed that this fuel form could increase by 2.3–2.4 times the thermal power output of a light weight radioisotope heater unit. These figures are for a single-size ( $500\ \mu\text{m}$ ) particles compact, assuming 10% and 5% helium gas release respectively, and a fuel temperature of 1723 K, following 10 years of storage. A binary-size (300 and  $1200\ \mu\text{m}$ ) particles compact increases the thermal power output of the RHU by an additional 15%. © 2001 Elsevier Science B.V. All rights reserved.

## Nomenclature

$a$	average fuel grain radius (m)
$b$	coefficient (Eq. (11)), $b = 1.5121 \times 10^{-2}\ (\text{m}^3\ \text{kg}^{-1})$
$D$	gas mass diffusion coefficient in fuel matrix ( $\text{m}^2\ \text{s}^{-1}$ )
$D'$	effective gas diffusion coefficient in fuel, $D' = D/a^2\ (\text{s}^{-1})$
$D_f$	diameter of fuel kernel (m)
$D_g$	average diameter of fuel grain (m)
$D_p$	outer diameter of coated fuel particle (m)
$F$	fraction of helium gas released from the fuel matrix that exerts pressure on outer coating

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$F^*$	release-to-birth rate ratio of radioisotope
$M$	molecular weight ( $\text{kg mol}^{-1}$ )
$n$	number of moles (moles)
$N_a$	Avogadro number ( $N_a = 6.0225 \times 10^{23}$ atoms $\text{mol}^{-1}$ )
$N_o$	Pu-238 atom density of as-fabricated plutonia fuel kernel (atoms $\text{kg}^{-1}$ )
$P$	pressure (Pa)
$q$	thermal power ( $W_{\text{th}}$ )
$q'''$	volumetric thermal power ( $W_{\text{th}} \text{ m}^{-3}$ )
$R_g$	perfect gas constant ( $R_g = 8.3143 \text{ J mol}^{-1} \text{ K}^{-1}$ )
$R_{\text{inner}}$	inner radius of ZrC coating (m)
$\mathcal{R}$	dimensionless stress factor of a spherical shell
$S_p$	geometrical surface area of as-fabricated fuel kernel ( $\text{m}^2$ )
$S_R$	effective gas release area in fuel kernel ( $\text{m}^2$ )
$T$	temperature (K)
$t$	time (s)
$t_{\text{PyC}}$	thickness of pyrolytic carbon inner layer (m)
$t_{\text{ZrC}}$	thickness of ZrC coating (m)
$T_{1/2}$	radioactive decay half life (s)
VOL	volume ( $\text{m}^3$ )
$Y_{\text{ZrC}}$	yield strength of ZrC (Pa)

*Greek*

$\alpha$	fraction of coarse spheres in a binary mixture at maximum packing
$\beta$	maximum packing volume fraction of 2-size spheres in compact
$\gamma$	open grain boundary porosity
$\varepsilon_f$	as-fabricated porosity of fuel kernel
$\varepsilon_f^{\text{open}}$	amount of open porosity in fuel kernel
$\varepsilon_{\text{PyC}}$	as-fabricated porosity of pyrolytic carbon layer
$\lambda$	radioactive decay constant ( $\text{s}^{-1}$ )
$\eta$	thermal-to-electric conversion efficiency
$\rho$	density ( $\text{kg m}^{-3}$ )
$\sigma_T$	maximum tangential tensile stress in ZrC coating layer (Pa)
$\Psi$	thermal power ratio, $q_{\text{CPFC-RHU}}/q_{\text{LWRHU}}$

*Subscript/superscript*

f	PuO <sub>2</sub> fuel
He	helium gas
m	exponent
max	maximum
Pu	plutonium
TD	theoretical density
1	coarse particles in a binary mixture fuel-compact
2	fine particles in a binary mixture fuel-compact

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