



# Design and testing of a separate-type lighting system using solar energy and cold-cathode fluorescent lamps

Jui-Piao Yang <sup>a,\*</sup>, Horng-Ching Hsiao <sup>b</sup>

<sup>a</sup> Department of Electrical Engineering, China Institute of Technology, Taipei, Taiwan 115, Taiwan, ROC

<sup>b</sup> Department of Electrical Engineering, National Taiwan University of Science and Technology, Taipei, Taiwan 106, Taiwan, ROC

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## Abstract

This paper presents a solar-powered lighting system, using cold-cathode fluorescent-lamps (CCFLs), with its battery-charging circuit and lamp-ignition circuit being separated so that its solar panels can be installed at any distance deemed necessary away from the lighting site in order to receive the maximum solar energy available. This system adopts the maximum-power point tracking (MPPT) method to control the power output of the solar panels and uses the zero-voltage switching (ZVS) DC–DC converter, as the charging circuit, to increase the panels' power generation efficiency and the charging circuit's conversion efficiency. The electronic ballast circuit for the CCFL is constructed with a half-bridge inverter, a resonant inductor, and a Rosen-type piezoelectric transformer, which forms a piezoelectric resonant-type inverter: to simplify the circuitry and to improve the power conversion efficiency, the ballast circuit is designed to directly step up the battery voltage in igniting the lamp. We also establish the transmission-parameter model for the piezoelectric resonant-type inverter to provide the base for the electric-power circuit design. Our experimental results indicate that the proposed system possesses some advantages, such as greater energy efficiency, circuitry simplicity, and so on, and is suitable for night lighting in house yards, parks and advertising panels.  
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**Keywords:** Cold-cathode fluorescent lamps (CCFLs); Electronic ballast; Maximum-power point tracking (MPPT); Zero-voltage switching (ZVS) DC–DC converter; Piezoelectric transformer; Piezoelectric resonant-type inverter

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\* Corresponding author.

E-mail addresses: [april4120@tp.edu.tw](mailto:april4120@tp.edu.tw) (J.-P. Yang), [hsiao@mouse.ee.ntust.edu.tw](mailto:hsiao@mouse.ee.ntust.edu.tw) (H.-C. Hsiao).

### Nomenclature and abbreviations

AHS	triggering signal of PMOS (V)
ALS	triggering signal of NMOS (V)
$d'_1, b'_1, c'_1, d''_1$	piezoelectric transformer's transmission parameters
$d''_1, b''_1, c''_1, d'''_1$	transmission parameters of resonant inductance
$A_{PT}$	piezoelectric transformer's voltage step-up ratio
CCFL	cold-cathode fluorescent lamp
$C_{1r}$	resonant capacitance of ZVS DC–DC converter (nF)
$C_{o1}, C_{pV}$	capacitances ( $\mu\text{F}$ )
$C_1$	primary capacitance of the piezoelectric transformer's equivalent-circuit (nF)
$C$	capacitance of piezoelectric transformer's equivalent-circuit (nF) (series connection of $r, L$ and $C$ )
$C_2$	secondary capacitance of piezoelectric transformer's equivalent-circuit (nF)
$C_o$	capacitance of CCFL's equivalent-impedance (nF) (parallel connection of $R_o$ and $C_o$ )
$C_p$	primary equivalent-capacitance converted by transformer from $C_2$ and $C_o$ (nF)
$C_s$	primary equivalent-capacitance converted by transformer from $C_2$ and $C_o$ (nF) (series connection of $R_s$ and $C_s$ )
$C_{o2}$	filter capacitance ( $\mu\text{F}$ )
$D_1$	main power diode of ZVS DC–DC converter
$D_{1r}$	auxiliary power diode of ZVS DC–DC converter
$D$	duty cycle of NMOS
$D_3$	half-wave rectified diode
div	division
$E, F, G, H$	transmission parameters of piezoelectric resonant-type inverter
$f_r$	piezoelectric transformer's resonant-frequency (kHz)
$f_o$	resonant frequency of the resultant circuit comprising of the piezoelectric transformer and CCFL (kHz)
$f$	switching frequency of inverter (kHz)
$I_{pV}$	solar-panel's output current (A)
$i_o$	CCFL's current (mA)
$L_1$	boost inductance of ZVS DC–DC converter ( $\mu\text{H}$ )
$L_{1r}$	resonant inductance of ZVS DC–DC converter ( $\mu\text{H}$ )
$L_s$	resonant inductance of piezoelectric resonant-type inverter ( $\mu\text{H}$ )
$L$	inductance of piezoelectric transformer's equivalent-circuit (mH)
MPPT	maximum-power-point tracking
NMOS( $Q_2$ )	N-channel metal-oxide-semiconductor field-effect transistor
$n$	ideal transformer's turn ratio of piezoelectric transformer's equivalent-circuit
OVP	over-voltage protection
OCP	over-current protection
PMOS( $Q_1$ )	P-channel metal-oxide-semiconductor field-effect transistor
$P_o$	CCFL's output power (W)
$P_{pV}$	solar panel's output power (W)

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