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Smooth trajectory generation for industrial robots performing high precision assembly processes

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ABSTRACT

Industrial robots conceived for high-precision assembly processes are demanded to match the best trade-off between precision and speed. This research presents a new approach for defining the motion profiles of robots, based on a smooth trajectory generation model. Execution time is minimized by a novel multi-variable optimization approach, taking into account the performance of each joint and the requirements of extremely precise assembly tasks. The proposed method, tested on a modular robot for the optoelectronics industry, provides jerk-bounded trajectories up to 39% faster compared to the best performing motion planning approaches, while offering the possibility to adapt these trajectories for degraded operating conditions.

1. Introduction and paper motivation

Industrial robots are demanded to target extremely challenging precision and reliability performance with agile and efficient architectures. In the assembly industry of high precision, the trade-off between repeatability and speed represents a key competitive leverage for robots. Targeting cutting edge precision while being versatile (at hardware and software levels) implies researching on topics ranging from the design of more solid mechatronic robot modules with close to zero backlash [1], the design of modular and scalable kinematic models which can match production evolution with reconfiguration [2], trajectory planning and path planning which can diversify the strategy to distribute the motion across the robotic chain [3], and finally the field of modular control architecture that can detect and match changes of the robot morphology along with performing a persistent monitoring of its health and behavior [4].

The present work investigates the topic of trajectory planning for industrial robots that require a very high level of motion smoothness while executing highly precise assembly tasks. The subject of trajectory planning is traditionally addressed from the temporal perspective [5,6], the motion smoothness perspective [7] or a mix of both aspects [8]. In the field of precision manufacturing, motion smoothness is a primary aspect. To this aim, many works rely upon the use of spline functions, optimized or constrained with various approaches [9,10]. Moreover, multiple-axis movements are often managed in the operations workspace [11], although the definition of trajectories in joint space can be, in some cases, a viable simplification that allows to implement smoother joint trajectories. In both cases, various authors proposed to achieve a higher degree of regularity by increasing the polynomial degree of the path or of the motion profile [12,13]. A non-polynomial family of smooth profiles in the joints space has been used in Ref. [14], in a movement synchronization strategy where all the joints phase their acceleration ramps on the slowest one, in a rather conservative way. A further limit for the robot motion capability is represented by the difficulty to adapt the motion planning strategies on the fly when a robot anomaly is detected at servo drives or CNC levels. As a result of that, the degrading phenomena of robots cannot be minimized or temporarily handled with a regenerative motion strategy that is optimized over the time.

The current work is motivated by the realization of ReRob I (Fig. 1), a serial robot characterized by 5 μm repeatability designed at SUPSI University [4], whose high-precision target level raises the necessity for smooth motion planning. ReRob I presents a high level of modularity in the mechanical structure, along with a decentralized control system architecture. By relying upon a set of Key Performance Indicators (KPIs), such control architecture allows to adapt the kinematic limits of each joint and in general the trajectory of the robot, depending on the detected performance status of the robotic modules.

In this work, the authors propose a multi-variable time optimization approach for motion planning, based on smooth jerk motion profiles. These are optimized taking into account both the specific robot task and the exact allocation of the specific joint models across the robotic chain, as described in Section 2.1. Fig. 1 shows an overview of ReRob I's kinematic adaptation scheme.

The rest of the paper is organized as it follows: Section 2 outlines the approach and the mathematical formulation; Section 3 describes the test setting and compares the proposed method with other state-of-the-art approaches; Section 4 summarizes the benefits of the approach and the future steps.

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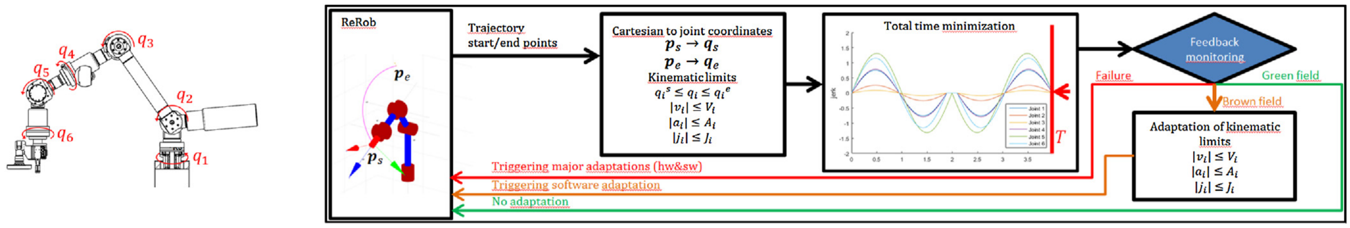

Fig. 1. Drawing of ReRob I configured as an anthropomorphic, spherical wrist manipulator (left panel) and sketch of ReRob I's trajectory planning and adaptation scheme (right panel).

2. Trajectory planning

The model detailed in the current section is based on the optimization of execution time by generating trajectories in the joint space, under range constraints for acceleration, velocity and jerk. Given the starting and ending coordinates of a movement, the method is independent from the underlying kinematic model, as it works only on the motion laws for joint displacements. The chosen type of parametric motion profile is the *sine-jerk* suggested in Ref. [15], applied to the motion of multiple joints. This parametric family allows to produce smooth motion profiles, while offering an easy way to control the maximum values of jerk, acceleration and velocity.

Sine-jerk motion profiles have already been applied to multiple joints movements in Ref. [14]. Our work presents a different approach, based on the simultaneous optimization of execution time on all joints, which overcomes some limitations of the existing one, thus enabling new features:

- In Ref. [14], all the trajectory phases (acceleration, constant velocity and deceleration) are synchronized across the joints, i.e. they begin and end at the same time. Our approach allows asynchronous accelerations and decelerations, and constrains only the total movement time. This largely extends the set of admissible solutions, possibly including faster ones.
- The method in Ref. [14] determines the acceleration/deceleration and constant velocity times for all the joints firstly by evaluating singularly their fastest acceleration ramp times and constant velocity times, then equalizing all of them to the largest values found. This conservative criterion is quite far from optimality. Our approach optimizes numerically the execution time by adapting acceleration times in the best possible way.

The trajectory planning module introduced in this work relies on the following assumptions:

- The considered robot manipulator performs mainly pick-and-place tasks associated to assembly processes where very smooth pick and place movements are required, to provide an accurate positioning of the gripped component.
- Rapid movements are performed between pre-pick and pre-place positions that do not require specific paths (e.g. linear) in the Cartesian workspace or avoidance of any obstacles. This implies that rapid point-to-point movements can be performed by trajectories designed in the joints space. A collision avoidance strategy, which is out of the scope of this work, could be introduced for example by iteratively adding intermediate waypoints to the trajectory.
- Though inspired by a specific configuration of ReRob I, i.e. a 6-degrees of freedom (DoF) anthropomorphic manipulator with spherical wrist, the proposed motion planning method has general purpose, and it can be adapted to any serial or parallel manipulator with arbitrary DoFs.

2.1. Model rationale for high precision manipulator

The industrial manipulator structure we refer to is constituted by a number of modular joints and links which form the kinematic chain. Each joint $i = 1, \ldots, n$, where the index i represents the serial position in the kinematic chain, is characterized by a specific joint type k_i. In particular, a typical anthropomorphic, spherical-wrist configuration can be assembled by using 2 different types of joints: a higher torque model for the first 3 axes and a smaller, lower torque model for the 3 wrist axes, yielding $k_1, k_2, k_3 = 1$ and $k_4, k_5, k_6 = 2$. Each joint has different velocity, acceleration and jerk ranges, depending on the type of joint and on its position in the kinematic chain.

Also the specific type of assembly task and the starting and ending positions may influence the kinematic parameters for each joint: for example, movements to be performed with the empty gripper may be realized at higher speeds and accelerations with respect to movements performed while carrying a component; moreover, long-reach trajectories, which are more stressful for the actuators, may require slower movements to keep oscillations within the required specifications. The task index $m = 1, \ldots, n_t$ allows then to differentiate control parameters between different segments of the work process. As mentioned before, this index depends on starting and ending Cartesian positions $\mathbf{p}_s$, $\mathbf{p}_e$ and task type h (e.g. pick, place, change tool, etc.), but for brevity the full dependence $m = m(\mathbf{p}_s, \mathbf{p}_e, h)$ will be omitted in the following. The task index influences the values of motion constraints (maximum jerk J^{MAX}, maximum acceleration A^{MAX} and maximum velocity V^{MAX}, as well as path destinations), while acceleration ramps will be optimized for each task.

2.2. Sine-jerk motion profile mathematical formulation

Positions $\mathbf{p}_s$ and $\mathbf{p}_e$ must be translated into a starting and ending position for each joint, using the proper kinematic inversion, to allow the generation of motion profiles for the joints. The algorithm we present in Section 2.3 generates trajectories in the joints space, providing motion profiles that are monotonic for each single joint. To generate joint motion profiles, we choose the expression of jerk as a function of time suggested in Ref. [15]. The proposed profile for a single motor, exemplified in Fig. 2, is

$$j(t) = \begin{cases} J\sin\left(\dfrac{2\pi}{\tau}t\right) & \text{for } t \in [0, \tau) \\ 0 & \text{for } t \in [\tau, \tau + T_V) \\ -J\sin\left(\dfrac{2\pi}{\tau}t\right) & \text{for } t \in [\tau + T_V, 2\tau + T_V], \end{cases} \tag{1}$$

where J is the jerk peak value, τ is the acceleration time and T_V is the constant velocity time.

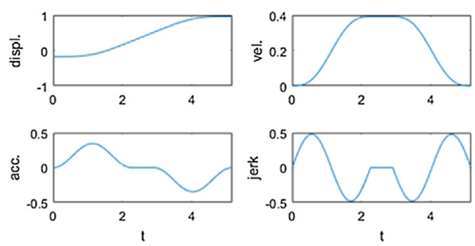

Fig. 2. Jerk, acceleration, velocity and displacement derived from the sinusoidal jerk model.

Notice that $2\pi/\tau$ represents the sine-wave angular frequency. This profile exhibits very high regularity, nonetheless it allows to parameterize the displacement, velocity and acceleration profiles by few, easily interpretable parameters, and to define their values by means of a proper optimization method.