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Expansion development planning of thermocracking-based bitumen upgrading plant under uncertainty



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ABSTRACT

Expansion development of upgrading plants is an important decision to make for the oil sands industry. In this paper, we propose a multistage stochastic expansion development method to tackle uncertain synthetic crude oil (*SCO*) and *CO*₂ tax prices. The linear decision rule based technique is applied to solve the proposed stochastic optimization model. Various analyses are conducted based on optimization results: (i) effects of the uncertainty set size, (ii) comparison of solutions for selected pessimistic, realistic, and optimistic scenarios, (iii) effects of different operating modes for an upgrading plant, and (iv) cost distribution. Results of this work demonstrate that the stochastic model provides a more flexible, economical, and robust solution negligibly compared to the *SCO* price. Finally, expansion development of the studied upgrading plant is economically beneficial even at the current market state.

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1. Introduction

Crude oil is the global dominant energy source and the reliance of the world economy on it is expected to continue for a long time. It is estimated that the worldwide demand of crude oil will reach 111 million barrels per day by 2040, and approximately 25% of it will be contributed by North America, including Canada and the United States (World Oil Outlook, 2014). Due to the increasing scarcity of conventional oil reserves, oil industries and governments are interested in unconventional oil resources. Note that oil reserves that cannot be accessed using conventional drilling techniques are referred as unconventional oil. These reserves (e.g., tight oil, oil shale and bitumen) need novel methods for extraction (Demirbas et al., 2017; Wang et al., 2016). After Saudi Arabia and Venezuela, Canada has the third largest oil reserves with proven 168 billion barrels (Woynillowicz et al., 2005). Furthermore, nearly 97% of total Canadian oil reserves are in the form of oil sands, which are mainly distributed in the Athabasca, Cold Lake, and Peace River areas in northern Alberta (Woynillowicz et al., 2005).

Unconventional oil production in Canada is continuously increasing. The oil sands bitumen production in Alberta is projected to reach 3.8 million barrels per day by 2022, which will be two times the production as of 2012 (Lazzaroni et al., 2016). While oil

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https://doi.org/10.1016/j.compchemeng.2018.01.007 0098-1354/© 2018 Elsevier Ltd. All rights reserved. price fluctuation affects profitability of the oil sands industry, important issue is how to adjust production and expansion planning under an uncertain market environment. Another major concern for the continuous development of the oil sands industry is the environmental management. Sustainable development with minimum environmental conservation is a concern of Alberta provincial and Canadian federal governments. To follow the international agreements (the United Nations Framework and Kyoto protocol), Canada is committed to mitigating its greenhouse gas (GHG) emissions. In Alberta, a carbon tax of \$15 per tonne of CO₂ was enacted in 2007 for the first time (Fact Sheet: Carbon Pricing Around the World, 2012). Recently, it was increased to \$20 and \$30 per tonne of CO₂ in 2016 and 2017 (Alberta Boosts Carbon Tax, 2015; Carbon Levy and Rebates, 2017). It is expected that the carbon tax rate will be increased; however, the exact future tax level is unknown. As it can be seen, the further development of the oil sands industry is accompanied with uncertainties in both the unpredictable oil price and changing environmental policies. Studying the development and expansion planning under uncertainties currently seems essential for the oil sands industry.

The uncertainty issue has received attention in various design and planning problems. The strategic planning of a bioethanolsugar supply chain was studied under demand uncertainty (Kostin et al., 2012). A two-stage multi-scenario mixed-integer linear stochastic programming approach was proposed, and a decomposition technique was applied to solve it based on the sample average approximation technique. It was further shown that the stochastic model lead to more robust solution compared to

Nomenclature		$\underline{\Omega}^{M}$	upper bound for the inlet to the upgrading plant $(\frac{tonne}{hr})$
Acronyms	5	0 ⁰	
ARMA	Auto Regressive Moving Average	$\underline{\Omega}_{p}^{Q}$	lower bound for percentile of capacity usage (%)
DP	Deterministic Problem	$\underline{\Omega}_{p}^{\hat{s}pec}$	lower bound for percentile of each product in fi-
DR	Diluent Recovery	- X = X	nal blend (%)
el	Electricity	$\underline{\Omega}_p^X, \overline{\Omega}_p^X$	
GHG	GreenHouse Gas		(bpd)
HGO	Heavy Gas Oil	$a_p \\ A_t^{SCO}$	gradient of linear capital cost equation
	Heavy Gas Oil HydroTreater	A_t^{SCO}	constant coefficients vector of reformulated
ht	Heat		ARMA model at year t
		b_p	intercept of linear capital cost equation (M\$)
HT	HydroTreater	b _p B ^{SCO}	constant coefficients scalar of reformulated ARMA
LDR LGO	Linear Decision Rule		model at year <i>t</i>
LGO LGOHT	Light Gas Oil	d	depreciation time (yr)
	Light Gas Oil HydroTreater	h	the coefficients vector of general uncertainty set
NPH	Naphtha Nachtha UadarTractar	ir	annual real debt interest rate (%)
NPHHT	Naphtha HydroTreater	OT	operating time (<i>hr</i>)
NPV	Net Present Value	P_t	truncate matrix at year t
SAGD	Steam-assisted gravity Drainage	r	discount rate (%)
SCO	Synthetic Crude Oil	UC ₁	unit conversion from cubic meter per hour into
SOR	Steam-Oil-Ratio	1	barrel per day $(\frac{bpd}{m^3})$
SP	Stochastic Problem		$\frac{m^3}{hr}$
st	Steam	UC ₂	unit conversion from \$ to M\$ $(\frac{M\$}{\$})$
TC	Thermocracker	W	coefficient matrix of general uncertainty set
		$z_{1-\alpha}$	$1 - \alpha$ quantile of standard normal distribution
Indices a	nd sets		-
$p \in \mathcal{P}$	set of operating units		variables
$u \in \mathcal{U}$	set of utilities	Λ	variable stemmed from dual counterpart of inequal-
$t\in\mathcal{T}$	set of time periods	6400V	ity constraint
$\mathcal{C}\in\mathcal{C}$	set of products	C_t^{CAPEX}	capital cost investment of year t (M\$)
\mathcal{MP}	subset of mixer-type units (NPHHT, LGOHT, HGOHT)	<i>Y</i> _{<i>p</i>, <i>t</i>}	binary capacity expansion decision for process p in
SP	subset of splitter-type units (<i>DR</i> , <i>TC</i>)		the year <i>t</i>
PC	subset of matching between product and associated	$M_{p,t}^{H2}$	mass flow rate of hydrogen in hydrotreater p at year
10	hydrotreater	<i>F</i> , <i>r</i>	$t \left(\frac{tonne}{hr}\right)$
	nyuloticatei	$M_{p,c,t}^{out}$	mass flow rate of outlet product <i>c</i> from splitter <i>p</i> at
Daramata	***	<i>p</i> , <i>c</i> , <i>t</i>	year $t \left(\frac{tonne}{hr}\right)$
Paramete	significance level	млin	
α		$M_{p,t}^{in}$	mass flow rate of inlet to splitter <i>p</i> at year $t \left(\frac{tonne}{hr}\right)$
$\alpha_{p,c}^{yield}$ $\alpha_{p}^{H_2}$	yield coefficient of splitter-type units	$M_{p,t}^{HTout}$	mass flow rate of outlet from hydrotreater p at year
$\alpha_p^{n_2}$	hydrogen requirement coefficients $(\frac{tonne}{m^3})$		$t \left(\frac{tonne}{hr}\right)$
α_p^{HT}	yield coefficient of mixers	$M_{p,t}^{H2}$	mass flow rate of hydrogen in hydrotreater p at year
$\beta_{p, u}^{P}$	energy requirements coefficient (<u>energy</u>)	<i>p</i> ,c	$t \left(\frac{tonne}{hr}\right)$
γ^{CO_2}	carbon tax economic coefficient $\left(\frac{\$}{tonne}CO_{2}\right)$	M ^{SCO}	total mass flow rate of SCO at year $t \left(\frac{tonne}{hr}\right)$
γ Y ^{Bitumen}			energy concumption of utility u at year $t \left(\frac{e^{nergy}}{hr} \right)$
	Bitumen price $(\frac{\$}{bbl})$	$E_{u, t}$	energy consumption of utility <i>u</i> at year $t \left(\frac{energy}{hr}\right)$
γ_u^E	energy requirements economic coefficients	$X_{p, t}$	capacity expansion of process p to be installed in pariod t (had)
	$\left(\frac{\$}{energy}\right)$		period t (bpd)
γ^{H_2}	hydrogen requirement economic coefficients	Q _{p, t}	total capacity of process p in period t (bpd)
	$\left(\frac{\$}{tonne}\right)$		
γ^{MAINEX}	maintenance economic coefficient		
γ^{SCO}	SCO price $(\frac{s}{bbl})$		ninistic model. The strategic investment planning of a
Γ	a scalar to control the uncertainty set size	-	luct, multi-period supply chain problem was investi-
δ_u^E	GHG emission coefficient of Energy sources	gated (Oliv	veira et al., 2013). To address the demand uncertainty,
ou		a two-stag	ge mixed-integer linear stochastic programming model
- 11	$\left(\frac{\text{tonne } \text{CO}_2}{\text{energy}}\right)$	with risk	consideration was taken into account to reduce the
δ^{H_2}	GHG emission coefficient of Hydrogen $\left(\frac{tonne CO_2}{tonne}\right)$	chances of	f very large objective function values during minimiza-
δεςο	GHG emission coefficient of SCO production	tion. A tv	vo-stage mixed-integer linear stochastic programming
	$\left(\frac{\text{tonne CO}_2}{\text{tonne}}\right)$		ed for the expansion planning of electricity generation
ϵ_t	uncertainties for SCO price		rk and Baldick, 2015). Various power generation tech-
ζt	uncertainties for CO ₂ tax price	niques (coal, combustion turbine, nuclear, combined cycle and	
θ_q	ARMA ARMA model coefficients		rator) were considered. The load and wind availabilities
		-	
ρ_p	density $\left(\frac{tonne}{m^3}\right)$		incertain parameters which were defined as independent
ϕ_p $\bar{\Omega}_t^{Investme}$	ARMA ARMA model coefficients		cally distributed random variables. Environmental regu-
S2t	· · · ·		cluding carbon tax and a renewable portfolio standard)
	period t (M\$)	-	osed on the model as well. This model was solved us-
		ing the I	shaped method based on the Monte Carlo simulation

ing the L-shaped method based on the Monte Carlo simulation.

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