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## Research Paper

# Day-to-night heat storage in greenhouses: 1 Optimisation for periodic weather



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Day-to-night heat storage using water tanks (buffers) is common practice in cold-climate greenhouses, where gas is burned during the day for carbon dioxide enrichment. In this study an optimal control approach is outlined for such a system, based on the idea that the virtual value (shadow price) of the stored heat, its ‘co-state’, could be used to guide the instantaneous control decisions. If this value is high, the system has an incentive to fill the heat storage (buffer), and vice versa if the co-state is low. The optimal co-state trajectory maximises the net income (performance criterion). To illustrate the method, a system description and a parameter-set roughly representative of tomato greenhouses in The Netherlands is used. The results, for daily-periodic weather, show: (1) The optimal co-state is constant (same value night and day), in contrast to the varying set-points and control fluxes. (2) The optimal solution is associated with minimum time on the storage bounds (minimum time of full or empty buffer). (3) The optimal virtual value (co-state) of stored heat is about the same as the actual cost of boiler heat during winter and about zero in summer. (4) The gain from installing a buffer is highest during spring and minimal in winter. (5) The intensive utilisation of the heat buffer in summer and its low utilisation in winter indicate that the justification of the heat storage practice, under the assumed conditions, is more the need for CO<sub>2</sub> enrichment in summer than the need for heating in winter.

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## 1. Introduction

In cold-climates, where natural gas is burned during the day to enrich greenhouses with carbon dioxide (CO<sub>2</sub>), water tanks (heat buffers) are often used to store extra daytime heat for heating at night (De Zwart, 1996; Salazar, Miranda, Schmidt, Rojano, & Lopez, 2014). Attempts to utilise this technique in

milder climates have also been reported (Bailey et al., 2012), although our calculations (not shown) do not seem to justify its use in mild climates. The inverse approach, of night-to-day storage of CO<sub>2</sub> in activated carbon, has also been tried (Sánchez-Molina, Reinoso, Ación, Rodríguez, & López, 2014).

There are several possible, and actual, configurations of such facilities; however, the focus of the present study is not on a particular configuration, but rather on an optimal

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Notation			
*	units may differ among vector elements	X	CO <sub>2</sub> flux, mol [C] m <sup>-2</sup> [ground] s <sup>-1</sup>
[ground]	greenhouse ground surface	<b>x</b>	vector of state variables, *
		Y	growth rate of salable fruit (yield), mol [fruit-C] m <sup>-2</sup> [ground] s <sup>-1</sup>
Symbols		β	temperature exponent of respiration, K <sup>-1</sup>
a	light extinction coefficient, m <sup>2</sup> [ground] mol <sup>-1</sup> [C]	Γ	gain from installing a buffer (≡J{S <sub>c</sub> } - J{0}), \$ m <sup>-2</sup> [ground]
B	Bowen (sensible to latent heat) ratio, -	ε	efficiency of heat storage, -
C	CO <sub>2</sub> concentration, mol [C] m <sup>-3</sup> [air]	η <sub>FH</sub>	heating coefficient of global (solar) radiation, J [heat] J <sup>-1</sup> [global]
c	specific heat of air, J [heat] kg <sup>-1</sup> [air] K <sup>-1</sup>	η <sub>FL</sub>	conversion factor solar energy to photosynthetic light, mol [PAR] J <sup>-1</sup> [global]
e	vector of exogenous (weather) variables, *	η <sub>HX</sub>	conversion factor heat to CO <sub>2</sub> , mol [C] J <sup>-1</sup> [heat]
F	global (solar) radiation flux, J [global] m <sup>-2</sup> [ground] s <sup>-1</sup>	η <sub>LX</sub>	conversion factor light to CO <sub>2</sub> (photosynthetic 'efficiency'), mol [C] mol <sup>-1</sup> [PAR]
f	sunlit leaf area index, m <sup>2</sup> [sunlit-leaf] m <sup>-2</sup> [ground]	ζ	fraction growth of saleable fruit out of total growth, -
f	vector function describing state rate-of-change, *	κ	temperature correction coefficient, K <sup>-2</sup>
g	running (control) costs, \$ m <sup>-2</sup> [ground] s <sup>-1</sup>	Λ	co-state of S, \$ J <sup>-1</sup> [heat]
H	heat flux, J [heat] m <sup>-2</sup> [ground] s <sup>-1</sup>	ρ	air density, kg [air] m <sup>-3</sup> [air]
ℋ	Hamiltonian, \$ m <sup>-2</sup> [ground] s <sup>-1</sup>	σ	leaf conductance to CO <sub>2</sub> , m <sup>3</sup> [air] m <sup>-2</sup> [sunlit-leaf] s <sup>-1</sup>
h	termination value, \$ m <sup>-2</sup> [ground]	τ	transmissivity of greenhouse-cover to light, -
J	performance criterion (objective function), \$ m <sup>-2</sup> [ground]	<b>Subscripts</b>	
L	photosynthetic light flux, mol [PAR] m <sup>-2</sup> [sunlit-leaf] s <sup>-1</sup> = mol [PAR] m <sup>-2</sup> [ground] s <sup>-1</sup>	A	dissipated to atmosphere
M	carbon content of crop, mol [C] m <sup>-2</sup> [ground]	B	supplied from boiler
N	growth rate of non-fruit organic matter, mol [C] m <sup>-2</sup> [ground] s <sup>-1</sup>	c	installed capacity
P	gross photosynthesis rate, mol [C] m <sup>-2</sup> [sunlit-leaf] s <sup>-1</sup>	D	day
p	gross photosynthesis rate at optimal temperature, mol [C] m <sup>-2</sup> [sunlit-leaf] s <sup>-1</sup>	d	discharging
p	vector of co-state variables, *	F	due to global (solar) radiation
q	temperature response of photosynthesis, -	f	final
R	respiration rate, mol [C] m <sup>-2</sup> [sunlit-leaf] s <sup>-1</sup>	G	to greenhouse
S	stored heat, J [heat] m <sup>-2</sup> [ground]	i	indoor
S <sub>D</sub>	daytime storage requirement, J [heat] m <sup>-2</sup> [ground]	max	maximum value
S <sub>N</sub>	nighttime storage requirement, J [heat] m <sup>-2</sup> [ground]	min	minimum value
s	slope of stored heat trajectory, J [heat] m <sup>-2</sup> [ground] s <sup>-1</sup>	N	night
T	air temperature, K, °C	o	outdoor
t	time, s	p	optimal for photosynthesis
U	overall heat transfer coefficient across greenhouse cover, J [heat]m <sup>-2</sup> [ground] K <sup>-1</sup> s <sup>-1</sup>	r	at reference temperature
u <sub>B</sub>	unit price of boiler heat, \$ J <sup>-1</sup> [heat]	S	heat storage (in buffer)
u <sub>Q</sub>	unit price of ventilation, \$ m <sup>-3</sup> [air]	T	total loss from greenhouse
u <sub>Y</sub>	unit market price of produce (fruit) dry matter, \$ mol <sup>-1</sup> [fruit-C]	t	on upper storage bound
u	vector of control variables, *	u	charging
		V	by ventilation
		<b>Acronyms</b>	
		D	Dimension
		PAR	Photosynthetically Active Radiation

strategy to control the operation of such systems. Attempts to solve the CO<sub>2</sub> enrichment problem in conjunction with heat buffers have been made before (Aikman, Lynn, Chalabi, & Bailey, 1997; Chalabi, Biro, Bailey, Aikman, & Cockshull, 2002). These, however, considered the heating needs (set-points) separately from CO<sub>2</sub> enrichment and did not treat the

heat flux in and out of the buffer as a control variable. Here the method of optimal control is followed (Pontryagin, Boltyansky, Gamkrelidze, & Mischenko, 1962), the basic idea being that the co-state of the stored heat, namely its current virtual (marginal, shadow) value, could be used to guide the instantaneous control decisions. If this value is high, the

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