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Generic functional modelling of multi-pulse auto-transformer rectifier units for more-electric aircraft applications

Tao YANG^{a,*}, Serhiy BOZHKO^a, Patrick WHEELER^a, Shaoping WANG^b, 6 Shuai WU^b 7

^a Department of Electrical and Electronic Engineering, University of Nottingham, Nottingham NG72RD, UK 8 9

^b School of Automation Science and Electrical Engineering, Beihang University, Beijing 100083, China

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Abstract The Auto-Transformer Rectifier Unit (ATRU) is one preferred solution for high-power AC/DC power conversion in aircraft. This is mainly due to its simple structure, high reliability and reduced kVA ratings. Indeed, the ATRU has become a preferred AC/DC solution to supply power to the electric environment control system on-board future aircraft. In this paper, a general modelling method for ATRUs is introduced. The developed model is based on the fact that the DC voltage and current are strongly related to the voltage and current vectors at the AC terminals of ATRUs. In this paper, we carry on our research in modelling symmetric 18-pulse ATRUs and develop a generic modelling technique. The developed generic model can study not only symmetric but also asymmetric ATRUs. An 18-pulse asymmetric ATRU is used to demonstrate the accuracy and efficiency of the developed model by comparing with corresponding detailed switching SABER models provided by our industrial partner. The functional models also allow accelerated and accurate simulations and thus enable whole-scale more-electric aircraft electrical power system studies in the future.

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Driven by the demand to optimize aircraft performance,

decrease operation and maintenance costs and reduce noise

pollution, the aircraft industry has been pushed towards the

concept of the More-Electric Aircraft (MEA). In the MEA,

many functions which are conventionally managed by hydrau-

lic, pneumatic and mechanical power, will be replaced with

devices driven by electrical power.^{1,2} Such replacement would

1. Introduction

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Corresponding author.

E-mail address: Tao. Yang@nottingham.ac.uk (T. YANG). Peer review under responsibility of Editorial Committee of CJA.

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reduce system weight and volume, increase overall reliability. 29 capability and maintainability, and provide higher durability 30 for aircraft operations.³ Aircraft power electronics have also 31 been affected by this trend. The need for power conversion 32 and driving equipment on-board has become significant. 33 Recently, the usage of AC-DC conversion has become a com-34 35 mon feature for aircraft power distribution systems. In general, there are two main types of this AC-DC power conversion: the 36 PWM active front-ends and passive multi-phase transformer 37 rectifiers. The former has seen increased application incorpora-38 tion such as electromagnetic actuators⁴ and electrical starter-39 generator applications.⁵ However, the latter seems to be the 40 41 main power source for high-power DC load such as aircraft Environment Control Systems (ECS) due to its simple struc-42 ture and high reliability. The civil aircraft has long been using 43 Transformer Rectifier Unit (TRU) to produce 28 VDC from 44 115 V, 400 Hz ACsources. However, recently the auto-45 46 transformer rectifier has received more attention in aerospace 47 industry due to its reduced kVA rating compared with TRUs.⁶

A number of possible ATRU topologies have been pro-48 posed during the last decade.⁷⁻¹³ These ATRUs can be catego-49 rized into 12-pulse types, 18-pulse types, 24-pulse types, etc., 50 according to the number of pulses in the rectified voltage or 51 in the line current during one fundamental cycle. Among these 52 topologies, the 18-pulse ATRU seems to be a preferable 53 option. This is due to the fact that it has higher power quality 54 55 than the 12-pulse type and less devices than the 24-pulse or other higher pulse type ATRUs. The 18-pulse ATRU is now 56 57 actually being used on-board B787, the Dreamliner, supplying power to the environment control system.¹⁴ 58

The 18-pulse ATRUs can be divided into symmetric and 59 asymmetric types depending on the symmetry of voltages on 60 the secondary side of the transformer. For symmetric 18-61 pulse ATRUs, the voltages on the secondary side of the auto-62 63 transformer are with the same magnitude (normally the same with the magnitude of voltage on the primary side) and have 64 an equal phase shift of 40° from each other. The load power 65 66 is equally shared by the three directly-connected diode bridges. For asymmetric 18-pulse ATRUs, however, the voltages on the 67 secondary side are of different magnitudes. The voltage phase-68 69 shift angle is also not necessarily 40°.

The increased power electronics and motor drives on-board 70 MEA are bringing significant modelling challenges due to its 71 wide variation in time constant. The challenge is to balance 72 the simulation speed against the model accuracy and this is 73 dependent on the modelling task. Four different modelling lay-74 75 ers are defined according to the modelling bandwidth, i.e. architectural models, functional models, behavioural models 76 and component models^{15,16} as shown in Fig. 1. 77

The architectural layer computes steady-state power flow 78 and is used for weight, cost and cabling studies. In the func-79 tional level, the system components are modelled to handle 80 81 the main system dynamics up to 150 Hz. The error of models 82 in this level should be less than 5% in respect of the beha-83 vioural model accuracy. The behavioural model uses lumpedparameter subsystem models and the modelling frequencies 84 can be up to hundreds of kHz. The component models cover 85 high frequencies, electromagnetic field and ElectroMagnetic 86 Compatibility (EMC) behaviour, and perhaps thermal and 87 mechanical stressing. The bandwidth of component models 88 can be up to MHz region if required.¹⁶ 89



Fig. 1 Multi-level modelling paradigm.16

This paper aims to develop a general functional model of 90 ATRUs which allows future engineers to study ATRUs in a 91 more efficient and effective way. The functional models allow 92 accelerated and accurate simulations and thus enable a whole-93 scale MEA Electrical Power System (EPS) studies in the 94 future. The developed ATRU model is based on the vector 95 concept and in the synchronous dq frame. This method has 96 been widely used in modelling electrical machines.^{16–18} 97

The remainder of the paper is organized as follows: Section 2 briefly outlines the operation of ATRUs; Section 3 gives details of the development of the proposed modelling technique; an 18-pule ATRU is used for the effectiveness and efficiency studies in Section 4; Section 5 draws the conclusions of the paper.

2. Operation principles

The design of multiphase transformer rectifiers has been well discussed in Ref. 19. The auto-transformer rectifiers normally comprise a phase-shift transformer and a set of three-phase diode bridges as shown in Fig. 2. The phase shift transformer is not necessarily an auto-transformer type. However, the auto-transformer is a preferred option due to its low kVA ratings. In this paper, we mainly focus on auto-transformer rectifier units.

As can be observed in Fig. 2, the auto-transformer is used 113 to create three sets of three-phase voltages on the secondary 114 side, i.e. (v_{a1}, v_{b1}, v_{c1}) , (v_{a2}, v_{b2}, v_{c2}) and (v_{a3}, v_{b3}, v_{c3}) . These 115 resultant 9 phases are then fed into three diode bridges supply-116 ing power to the dc link. At each instant of time, there are two 117 diodes conducting. These two conducting diodes allow the lar-118 gest line-to-line voltage to be applied to the DC side. We refer 119 to the ATRU system shown in Fig. 2 as a "3-9-DC" system. 120 For some ATRUs, especially asymmetric ones, the voltage 121 sources on the primary side of the transformer also feed 122



Fig. 2 General auto-transformer rectifier units.

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