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## Development and experimental study of a small-scale compressed air radial inflow turbine for distributed power generation



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#### HIGHLIGHTS

• Proposing methodology for developing small-scale RIT as expander of CAES and ORC.

• 1D modelling enables estimation of turbine performance and obtaining key geometry.

• Turbine efficiency improved from 81.3% obtained by 1D model to 84.5% obtained by CFD.

• CFD predicts turbine efficiency and power with accuracy of ±16% and ±13% compared to tests.

#### ARTICLE INFO

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#### ABSTRACT

With ever increasing demand on energy, disturbed power generation utilizing efficient technologies such as compressed air energy storage (CAES) and organic Rankine cycle (ORC) are receiving growing attention. Expander for such systems is a key component and its performance has substantial effects on overall system efficiency. This study addresses such component by proposing an effective and comprehensive methodology for developing a small-scale radial inflow turbine (RIT). The methodology consists of 1-D modelling, 3-D aerodynamic investigation and structural analysis, manufacturing with pioneering technique and experimental testing for validation. The proposed 1-D modelling was very effective in determining the primary geometry and performance of turbine based on parametric studies of turbine input design variables. However with CFD analysis, it was shown that more efficient turbine geometry can be achieved that not only provides more realistic turbine performance by capturing the 3-D fluid flow behaviour but also improves turbine efficiency with the aid of parametric studies of turbine geometry parameters. Turbine efficiency was improved from 81.3% obtained from 1-D modelling to 84.5% obtained by CFD. Accuracy of the CFD model was assessed by conducting experiments on the RIT manufactured with stereolithography technique. The CFD model can predict turbine efficiency and power with accuracy of ±16% and ±13% respectively for a wide range of tested operating conditions. Such results highlights the effectiveness of the proposed methodology and the CFD model can be used as benchmarking model for analyses of small-scale RITs. Besides, it was shown that for such applications, the novel manufacturing technique and employed material are very effective for producing prototypes that assist design decisions and validation of CFD model with reasonable accuracy at reasonable cost and in timely manner.

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## 1. Introduction

Nowadays energy is a key factor in the global economy and the effectiveness of energy generation and consumption processes has remarkable impacts on our society and environment. Following the international energy agency (IEA) report [1], extending the current

\* Corresponding author. E-mail addresses: kiyarash.rahbar@gmail.com, kxr965@alumni.bham.ac.uk trend of energy consumption and energy efficiency to 2050 yields a growth of 70% and 60% in the global energy demands and emissions respectively compared to 2011. The associated emissions result in a long-term global average temperature rise of 6 °C by 2050 which can result in potentially devastating consequences such as climate change and energy security. IEA (2014) suggested an effective scenario called "2DS" which offers a vision for a sustainable energy system that reduces  $CO_2$  emissions to maintain the global temperature rise within 2 °C by 2050 and to limit increases in energy demand by 25% and cut emissions by 50%. This

<sup>(</sup>K. Rahbar).

### Nomenclature

Symbols		ω	rotational velocity (RPM)
Α	area (m <sup>2</sup> )		
b	blade height (m)	Subsci	ripts
BK	blockage factor (–)	1–5	stations across turbine
С	absolute flow velocity (m/s)	abs	absolute
C <sub>nozzle</sub>	nozzle chord length (m)	b	back plate
$C_p$	specific heat capacity at constant pressure (J/kg K)	cfg	centrifugal
$C_{\rm s}$	spouting velocity (J/kg) <sup>-1</sup>	Cor	coriolis
d	diameter (m)	f	friction
$d_{hyd}$	hydraulic diameter (m)	hub	rotor hub
EK	expansion ratio (-)	j	counter
J	friction coefficient (-)	m	meridional direction
Jcurve h	turbine iniction factor (-)	r	radial
11	ential specific onthalmy drop (1/kg)	ref	reference
$\Delta \Pi_{actual}$	ideal specific enthalpy drop (I/kg)	rel	relative
$\Delta n_{ideal}$	anthalpy drop due to losses (I/kg)	rms	root mean square
∠In <sub>losses</sub> I	rothalpy (I/kg)	rotor	rotor
l V	coefficient (_)	s .	isentropic
к 1	length (m)	sonic	sonic velocity (speed of s
1	hydraulic length (m)	X	axial direction
<sup>t</sup> hyd	mass flow rate $(kg/s)$	stage	turbine inlet to turbine o
Ma	Mach number (_)	stat	static
N	specific speed (_)	t	total, stagnation
$\Omega_{\rm s}$	nozzle throat width (m)	tip	rotor tip
P	pressure (Pa)	ts 0	total to static
R	gas constant (I/kg K)	θ	tangential direction
Ro	universal gas constant ((I/(k mol))	c	• ,
RR	relative roughness (m)	Supers	scripts
Re	Reynolds number (–)	I	matrix transpose
r	radius (m)	_	average
r	location vector (m)		
r <sub>c</sub>	mean radius of curvature (m)	Mathe	ematical operators
S	entropy (J/kg K)	V	Vector operator $\left \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z}\right $
$S_E$	energy source (kg/(m s <sup>3</sup> ))	$\otimes$	dyadic operator (terisor p
$S_M$	momentum source ((kg/(m <sup>2</sup> s <sup>2</sup> ))		
Snozzle	nozzle blade pitch (m)	Acrony	yms
Т	temperature (K)	CAES	compressed air energy st
t	time (s)	CAD	computer alded design
U	rotor blade velocity (m/s)		computational nult dyna
U	vector velocity $\boldsymbol{U}_{x,y,z}$ (m/s)		controlized neur genera
W	relative flow velocity (m/s)		distributed power genera
W	molecular weight (kg/mol)		datum universal interface
Z	Blade number (-)	FFS	engineering equation solv
		FFA	finite element analysis
Greek let	ters	GGI	general grid interface
α	absolute flow angle with respect to radial (degree)	IFA	international energy ager
β	relative flow angle with respect to radial (degree)	LE	leading edge
γ	specific heat capacity ratio (–)	MOGA	A multi-objective genetic a
0	Identity matrix (-)	ORC	organic Rankine cycle
3	clearance (m) $(1x_1/x_2, x_2^2)$	PS	pressure surface
ζ.	shear stress tensor (kg/m s <sup>-</sup> )	RANS	Revnolds-averaged Navie
<i>1</i>	thermal conductivity (W/m K)	RIT	radial inflow turbine
л П	dynamic viscosity $(kg/(m s))$	RPM	revolutions per minute
ր D	isentronic velocity ratio $(-)$	SS	suction surface
0	density $(kg/m^3)$	SST	shear stress transport
ν σ	solidity (-)	TE	trailing edge
0 0	flow coefficient (–)		
$\hat{\psi}$	loading coefficient (-)		
T			

strategy creates a framework for a future sustainable energy systems which are expected to be smarter, renewable oriented, integrated, well-regulated and more distributed.

lis on hub ter dional direction ence ve mean square ropic velocity (speed of sound) direction ne inlet to turbine outlet stagnation tip to static ential direction ix transpose ige perators or operator  $\begin{bmatrix} \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \end{bmatrix}$ ic operator (tensor product) pressed air energy storage outer aided design outational fluid dynamics ined heat and power alized power generation buted power generation n universal interface neering equation solver element analysis

- ral grid interface,
- national energy agency
- ng edge
- i-objective genetic algorithm
- nic Rankine cycle
- ure surface
- olds-averaged Navier-Stokes
- l inflow turbine
- utions per minute
- on surface
- stress transport
- ng edge

Improvements in energy efficiency have significant contribution to the "2DS" scenario. For example, power in the traditional electrical grid (or centralized power generation) followed one

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