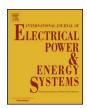
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Primary frequency control and dynamic grid support for vehicle-to-grid in transmission systems



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ABSTRACT

Because of vehicle-to-grid (V2G) growth, the provision of ancillary services by V2Gs is now required in the most recent network codes. A lack of primary frequency control (PFC) and dynamic grid support (DGS) in V2Gs could thus be detrimental to power system stability. This research presents a detailed V2G model with a hybrid energy storage system (HESS). The main contribution of the model is the simultaneous provision of PFC and DGS at its plug-in terminal. PFC includes both droop response (DR) and inertial response (IR). Accordingly, a frequency management system (FMS) determines the command of the V2G converter control for PFC without disturbing the scheduled charging-discharging. Simultaneously, this control enables DGS. The design of a new model for connecting V2Gs at transmission level allows the assessment of power system stability. This research study analysed the stability of an IEEE 39 bus system with 30% V2G penetration after critical contingencies. Various strategies for providing ancillary services in V2Gs (DGS and/or PFC) were compared in two scenarios defined by extreme V2G operating modes (as load or generator) at different locations. An analysis of the impact of each ancillary service as well as their interaction was performed to measure their influence on both system stability and critical operating variables of V2Gs. The results showed that system stability remained almost invariable when the V2Gs included PFC (DR+IR) and DGS.

1. Introduction

The new concept of V2G means that electric vehicles (EVs) should not only be regarded as passive assets, but also as a converter-based active generation. In general, an excessive and uncontrolled penetration of a converter-based distributed generation (DG) in power systems along with a partial replacement of traditional centralized generation reduces the available rotational inertia in power systems [1–6] and can cause a lack of DGS [2,7]. In order to ensure transient stability in power systems, the latest network codes and standards [8–13] recommend or require generating units (including those based on static converters, e.g. V2Gs) to synthetically inherit frequency support strategies from conventional generation and also provide DGS. In this context, V2Gs should receive operation references from the corresponding transmission system operator (TSO), mainly in the form of active and reactive power commands for providing different ancillary services, e.g. PFC [8,9,11–13] and DGS [8,9,11–13].

In recent years, much research has focused on the provision of PFC by EVs in electrical systems [14–40]. Recently, this provision by static a converter-based DG, though not specifically with EVs, has been a major

research focus [41,42]. As a result, the impact of EVs providing PFC on the transient stability of an electrical system can be characterised by the following EV-dependent factors: (i) EV penetration level [14,21-23,25]; (ii) location [38]: (iii) frequency control in the [15-18,20-22,25,28-30,32,33-35,38]; (iv) EV battery charger topology and its charging protocol [21,23,26-28,32,33,36,38]; (v) management of the state of charge (SOC) of an EV battery [16,18,27,29,30,33,38]; (vi) EV load model [24,26,34,39,40]; (vii) EV battery parameters [31,38]; (viii) use of a fast-response HESS embedded in the EV [19,32]; (ix) EV power variation limit for PFC (and droop coefficient [21]). Moreover, there are system-dependent factors that can have an impact on resulting transient stability: (i) medium voltage (MV) and low voltage (LV) lead conductors for the EV (aggregate model of EVs at MV or high voltage [HV] level) [21,25]; (ii) level of detail for modelling the power system, i.e., simplified vs. detailed system. Furthermore, any study of this impact should clearly differentiate outcomes in non-large electrical systems (e.g. microgrids [15,17,18,41,42], small island systems [20,23,26,33,38,39], and primary distribution systems [19,25,31,32,36]) as compared to large electrical systems (e.g. transmission systems [16,21,22,24,25,27–29,30,34,35,40]). Nonlinear interactions in non-large vs. large systems [43,44] involve

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Nomenclature		accuracy	
		TS-LV2GU # i connected to the transmission bus # i	
Abbreviations		и	voltage
DCMC	hidinational changing management anatom	$V2G_{Bi\#j}$	V2G connected to the <i>Bi</i> th,# <i>j</i> bus
BCMS	bidirectional charging management system	Comphala	
DG	distributed generation	Symbols	
CC	constant current	~	avmonant goofficient
CV	constant voltage	α	exponent coefficient
DGS	dynamic grid support	γ <i>v2G</i>	penetration level of V2G into the grid
DR	droop response	ζ	damping ratio overshoot ratio
EV	electric vehicles	ς Λ.ε	
FMS FRTC	frequency management system	Δf	frequency deviation frequency response insensitivity
HESS	fault-ride through capability	$\Delta f_{RI} \ \Delta f_{SS}$	steady-state frequency deviation
IR	hybrid energy storage system inertial response	Δyss Δp	change in active power
LCL	inductor-capacitor-inductor		
	<u>-</u>	Δp _{cmd}	rate of power variation of the V2G for PFC normalized by
PFC	, HV low voltage, medium voltage, high voltage	μ	the nominal charging power
PI	primary frequency control proportional-integral	o 50	C_{bat_j} ijth correlation coefficient for SOCs of ith and jth
PLL	phase-locked loop	$\rho_{SOC_{bati}}$, So	batteries
SC	supercapacitor		batteries
SOC	state of charge	Indices: S	lubscripts
TSO	transmission system operator	271410001 0	4000, P.B
	GU load and V2G unit at transmission-scale	av	average
V2G	vehicle-to-grid	bat	battery
V2G V2GC	V2G charger	cmd	command
V20C	v2G Charger	d-axis	at d axis
Variable	oc .	DC	at DC-link
variable	S.	DC-AC	to refer to DC-AC converter
С	capacitor	DR	droop response
f	frequency	f	at AC LCL filter
$G_{\#i}$	conventional generating unit #i connected to the trans-	g	grid
O#1	mission bus $\#i$	HESS	hybrid energy storage system
Н	inertia constant	IR	inertial response
i	current	L	inductor
K	adaptive gain	lo	lower
L	inductor	max	maximum
	(LRC_{IR}) limit rate of the change in active power due to DR	min	minimum
LITODR ((IR)	n	at nominal condition
m	exponential coefficient	PFC	primary frequency control
p	active power	q-axis	at q axis
$p_{\cdots-cmd}$	active power command of	ref	at reference condition
	-max/min maximum/minimum limit of power variation of	sc	supercapacitor
1110-120	V2G for PFC	scd	at scheduled condition
P	base capacity of power	ир	upper
q	reactive power	V2G	vehicle-to-grid
R	droop coefficient		
SOC	state of charge	Indices: S	Superscripts
S_{wi}	ith switch		
T	temperature	*	measured value
T_D	time constant associated with frequency derivate mea-	+	to refer to the aggregated approach when providing DGS
-	surement accuracy	\odot	to refer to commands under adaptive control
T_{HF1}	time constant associated with high-pass filter 1	c	at charging condition
	$_{F2)}$ time constant associated with low-pass filter 1 (2)	d	at discharging condition
T_P	time constant associated with frequency measurement		

different impacts. Therefore, the impact of the models/controls for PFC provision by EVs in non-large electrical systems cannot be extrapolated to transmission systems.

Frequency control in EVs includes simple approaches based on the sudden disconnection of EVs [21,35], a constant droop control [17,25,33-35], or an enhanced approach based on an adaptive droop control [27,29,30,33,38]. This control may also include a participation factor in the PFC that would facilitate the incorporation of various EV

characteristics such as battery SOC management [16,22,25,27,29,30,38] and/or battery charging protocol [38].

Associated EV battery charger topology and charging protocols are the following: (i) a unidirectional EV charger [16,28,33,40]; (ii) a bidirectional EV charger with a charging protocol [45] limited to constant current (CC) charging [17,18,23,26,32,38].

In the literature, EV load models are based on a simplified exponential load model (exponent α [40]) which may not be accurate: (i)

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