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Experimental And Numerical Analysis Of Modelling Of Solar Shading

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Abstract

The use of solar shading in future low energy office buildings is essential for minimizing energy consumption for building services, while maintaining thermal conditions. Implementing solar shading technologies in energy calculations and thermal building simulation programs is essential in order to demonstrate the effect of adaptive solar shading. In order to document the benefits of the shading technology, the description of the shading device in the thermal building simulation software must be described at a reasonably accurate level, related to the specific solar shading device.

This research presents different approaches for modeling solar shading devices, demonstrating the level of accuracy in relation to measurement conducted in a full-scale façade test facility at Aalborg University. The research bridges the gap between increased complexity of solar shading technologies and the use of these technologies in thermal building simulation software.

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1. Introduction

In order to reach zero-energy buildings for future office buildings, the use of adaptive envelope technologies is a necessity. The use of adaptive solar shading enables the control of irradiance in order to minimize energy demand for cooling, maximize passive solar heating for a reduction in energy demand for heating and optimize light transmittance for minimizing energy demand for artificial lighting while avoiding glare. As the user-pattern of office buildings tends to follow the same pattern as irradiation, presence during daytime hours, and away during night time hours, the cooling demand for office buildings is created as a sum of the internal heat load from people, equipment and lighting and external the heat load. The latter consists primarily of irradiance. The contribution of heat load from high outdoor

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temperatures is a function of the facades heat transfer coefficient. As the building's façade become more airtight and the maximum requirements for the structural parts U-value are tightened, the effect of high outdoor temperatures in relation to the cooling demand is considered a minimum.

Use of solar shading technologies for lowering energy demand for cooling is described in [1] as being part of a solution for lowering the energy transport through the façade, which potentially can reduce the cooling demand to near 0 kWh/m² pr. yr. The use of dynamic solar shading is a necessity for reducing the energy demand for cooling demand whilst maintaining a high level of passive solar heating. Furthermore the use of dynamic solar shading enables a high daylight level within the perimeter of the façade. [2] describes the potential of using static and dynamic solar shading for reducing the energy demand for cooling and artificial lighting.

The product development of solar shading is tested in a great deal when looking across the literature. The performance of individual solar shading technologies is shown, but as described in [3] the need for standardization of the calculation procedure is needed for documentation of solar shading technologies. [3] reviews the different methodologies for describing the optical properties of solar shading. In general there is agreement in the modeling of the direct-direct shading coefficient using the geometric method. The direct diffuse shading coefficient is modeled through the use of view factors between surfaces.

There is a gap in the current knowledge of solar shading technologies when describing these in thermal building simulation programs. The typical description of solar shading technologies are described as a function of incident angle [4]. The understanding of the performance of solar shading technologies from experiments compared with different detailing levels of the solar shading technologies is necessary.

The goal of this paper is thus to test different detailing methodologies for description of solar shading technologies in thermal building simulation software comparing the calculations with full scale experiments. The solar shading combined as a total shading factor or split into diffuse and direct shading factors and furthermore described as a fixed factor, as a function of incident angle, or absolute solar position will be analyzed. The description of the shading coefficient using different methodologies for description of the radiation from the different cloud covers will be investigated.

2. Method

The total shading factor is calculated as shown in Eq. (1), calculated as and irradiance weighted fraction of the irradiance reaching the façade including and excluding shading.

$$F_s = \frac{F_{S_b} I_b + F_{S_d} I_d + I_r}{I_b + I_d + I_r} \quad (1)$$

where F_s is solar shading factor, F_{S_b} is direct solar shading factor, F_{S_d} is diffuse solar shading factor, I_b is direct incident irradiance, I_d is diffuse incident irradiance, I_r is reflected incident irradiance.

The shading factor for direct radiation is calculated by geometric calculation of sunlit area versus total area as shown in Eq. (2). The calculation of the sunlit area is a sum of the direct-direct radiation and direct-diffuse radiation transmitted through the solar shading.

$$F_{S_b} = \frac{A_{w,s}}{A_w} \quad (2)$$

Where $A_{w,s}$ is shaded window area A_w is total window area.

The direct-direct irradiance is calculated based on the fraction of the irradiance being transmitted directly through the solar shading, relating the directly sunlit surface area with the total surface area. The calculation of the direct-diffuse irradiance is calculated based on the shading materials optical properties and view-factor between the shading surfaces and the glazing. The calculation process is shown in Eq. (3) and (4).

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